

Table 2-17
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (UNWELDED)

<u>Axial Tension</u>	Section	F/Ω	6005A - T61 B221 0.000 to 1.000 in. thick	
axial tension stress on net effective area	D.2b	19.5		
axial tension stress on gross area	D.2a	21.2		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	11.7	$F_{ly} =$	35 k/in ²
<u>Bearing</u>				
bolts or rivets on holes	J.3.6a, J.4.6	39.0	$F_{cy} =$	35 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	25.9	$F_{tu} =$	38 k/in ²
screws in holes	J.5.5.1	25.3	$E =$	10,100 k/in ²
			$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression - member buckling</u>	E.2	kL/r	21.2	17.8	$0.00047 \lambda^2 - 0.232\lambda + 25.2$	66	$51,352/\lambda^2$
<u>Flexure - lateral-torsional buckling</u>	F.4	see F.4.2	-	see F.4		66	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	21.2	6.7	$27.3 - 0.910 \lambda$	12	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	21.2	6.7	$27.3 - 0.910 \lambda$	10.5	$186/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	21.2	20.8	$27.3 - 0.291\lambda$	33	$580/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	21.2	17.8	$23.9 - 0.149\lambda$	66	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	21.2	27.6	$26.2 - 0.944 \lambda^{1/2}$	141	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	21.2	33.3	$27.3 - 0.182\lambda$	52	$928/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	31.8	33.1	$40.5 - 0.262\lambda$	77	$1,563/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	31.8	6.1	$40.5 - 1.412\lambda$	19	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	31.8	74.2	$40.5 - 0.117\lambda$	173	$3,502/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$39.3 - 2.70 \lambda^{1/2}$	55.4	$26.2 - 0.944 \lambda^{1/2}$	141	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	33.3	see B.5.5.5	61	$834/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	12.7	35.3	$16.5 - 0.107\lambda$	63	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	12.7	14.7	$16.5 - 0.257\lambda$	26	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	12.7	62.5	$21.5 - 0.140\lambda$	63	$50,264 / \lambda^2$
<u>Torsion - pipes and round or oval tubes</u>	H.2.1	λ_p^*	12.7	35.3	$16.5 - 0.107\lambda$	63	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$

Table 2-20
ALLOWABLE STRESSES F/Ω (k/in²) FOR BUILDING-TYPE STRUCTURES (UNWELDED)

<u>Axial Tension</u>	Section	F/Ω	6063 - T5	B221 0.000 to 0.500 in. thick
axial tension stress on net effective area	D.2b	11.3	6063 - T52	B221 0.000 to 1.000 in. thick
axial tension stress on gross area	D.2a	9.7		
<u>Shear or torsion</u>				
Shear or torsion rupture	G, H.2	6.8	$F_{ty} =$	16 k/in ²
<u>Bearing</u>				
bolts or rivets on holes	J.3.6a, J.4.6	22.6	$F_{cy} =$	16 k/in ²
bolts on slots, pins on holes, flat surfaces	J.3.6b, J.6.5, J.8	15.0	$F_{tu} =$	22 k/in ²
screws in holes	J.5.5.1	14.7	$E =$	10,100 k/in ²
			$k_t =$	1

	λ	F/Ω for $\lambda \leq \lambda_1$	λ_1	F/Ω for $\lambda_1 < \lambda < \lambda_2$	λ_2	F/Ω for $\lambda \geq \lambda_2$	
<u>Axial Compression - member buckling</u>	E.2	kL/r	9.7	18.8	$0.00008 \lambda^2 - 0.065\lambda + 10.9$	99	$51,352/\lambda^2$
<u>Flexure - lateral-torsional buckling</u>	F.4	see F.4.2		-	see F.4	99	$60,414/\lambda^2$
<u>Elements - Uniform Compression</u>							
flat elements supported on one edge in columns whose buckling axis is not an axis of symmetry	B.5.4.1	b/t	9.7	8.2	$11.8 - 0.260 \lambda$	19	$2,417/\lambda^2$
flat elements supported on one edge in all other columns and all beams	B.5.4.1	b/t	9.7	8.2	$11.8 - 0.260 \lambda$	15.9	$122/\lambda$
flat elements supported on both edges	B.5.4.2	b/t	9.7	25.6	$11.8 - 0.083\lambda$	50	$382/\lambda$
flat elements supported on both edges and with an intermediate stiffener	B.5.4.4	λ_s	9.7	18.8	$10.5 - 0.044\lambda$	99	$60,414/\lambda^2$
round hollow elements	B.5.4.5	R_b/t	9.7	36.7	$11.6 - 0.320 \lambda^{1/2}$	275	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.4.6	λ_{eq}	9.7	41.0	$11.8 - 0.052\lambda$	80	$611/\lambda$
<u>Elements - Flexural Compression</u>							
flat elements supported on both edges	B.5.5.1	b/t	14.5	36.1	$17.2 - 0.072\lambda$	119	$1,017/\lambda$
flat elements supported on tension edge, compression edge free	B.5.5.2	b/t	14.5	6.7	$17.2 - 0.389\lambda$	29	$4,932/\lambda^2$
flat elements supported on both edges and with a longitudinal stiffener	B.5.5.3	b/t	14.5	81.0	$17.2 - 0.032\lambda$	266	$2,280/\lambda$
pipes and round tubes	B.5.5.4	R_b/t	$17.5 - 0.917\lambda^{1/2}$	95.2	$11.6 - 0.320\lambda^{1/2}$	275	$3,776/(\lambda k_n)^\dagger$
flat elements - direct strength method	B.5.5.5	λ_{eq}	M_{np}/S_{xc}	41.0	see B.5.5.5	93	$549/\lambda$
<u>Elements - Shear</u>							
flat elements supported on both edges	G.2	b/t	5.8	43.6	$7.2 - 0.031\lambda$	96	$38,665/\lambda^2$
flat elements supported on one edge	G.3	b/t	5.8	18.2	$7.2 - 0.73\lambda$	40	$6,713/\lambda^2$
pipes and round or oval tubes	G.4	λ_p^*	5.8	87.3	$9.3 - 0.040\lambda$	96	$50,264/\lambda^2$
<u>Torsion - pipes and round or oval tubes</u>	H.2.1	λ_p^*	5.8	43.6	$7.2 - 0.031\lambda$	96	$38,665/\lambda^2$

* $\lambda_p = 2.9(R_b/t)^{5/8}(L/R_b)^{1/4}$
 $\dagger k_n = (1 + \lambda^{1/2}/35)^2$